

Research Article

AQUACOAST: A Simulation Tool to Explore Coastal Groundwater and Irrigation Farming Interactions

Jaime Martínez-Valderrama ¹, **Javier Ibáñez**,² and **Francisco J. Alcalá** ^{3,4}

¹Department of Ecology & Multidisciplinary Institute for Environment Studies “Ramón Margalef”, University of Alicante, 03690 San Vicente del Raspeig, Alicante, Spain

²Departamento de Economía Agraria, Estadística y Gestión de Empresas, Universidad Politécnica de Madrid, 28040 Madrid, Spain

³Instituto Geológico y Minero de España (IGME), 28003 Madrid, Spain

⁴Instituto de Ciencias Químicas Aplicadas, Facultad de Ingeniería, Universidad Autónoma de Chile, 7500138 Santiago, Chile

Correspondence should be addressed to Jaime Martínez-Valderrama; jaime.mv@ua.es

Received 10 January 2020; Accepted 28 April 2020; Published 14 May 2020

Academic Editor: Cristian Mateos

Copyright © 2020 Jaime Martínez-Valderrama et al. This is an open access article distributed under the Creative Commons Attribution License, which permits unrestricted use, distribution, and reproduction in any medium, provided the original work is properly cited.

In the framework of coastal groundwater-dependent irrigation agriculture, modelling becomes indispensable to know how this renewable resource responds to complex (usually not conceptualized nor monitored) biophysical, social, and economic interactions. Friendly user interfaces are essential to involve nonmodeling experts in exploiting and improving models. Decision support systems (DSS) are software systems that integrate models, databases, or other decision aids and package them in a way that decision makers can use. This paper addresses these two issues: firstly with the implementation of a System Dynamics (SD) model in Vensim software that considers the integration of hydrological, agronomic, and economic drivers and secondly with the design of a Venapp, push-button interfaces that allow users access to a Vensim model without going through the Vensim modelling environment. The prototype designed, the AQUACOAST tool, gives an idea of the possibilities of this type of models to identify and analyze the impact of apparently unrelated factors such as the prices of cultivated products, subsidies or exploitation costs on the advance of saltwater intrusion, and the great threat to coastal groundwater-dependent irrigation agriculture systems.

1. Introduction

A large proportion of the world's population depends on groundwater resources [1]. Groundwater accounts for as much as 33% of the global freshwater demand and is increasing [2]. This resource is especially crucial in regions where the surface water network does not cover a fraction of the freshwater demand at least, such as in many coastal drylands [3]. In these areas, aquifers play a critical role in sustaining the economy and the environment [4], but water scarcity has led to high groundwater abstraction rates to supply the increasing urban, tourism, industrial, and agriculture demands, thus adding stress to groundwater bodies [5, 6]. The cases with alarming signs of groundwater quantity depletion and quality degradation do not stop increasing [7].

Groundwater degradation in coastal drylands is often the result of complex interactions between global driving forces

and human-induced actions [8, 9]. Global climate scenarios forecast high evaporation rates and lower high-salinity aquifer recharge rates [10]. Some human-induced actions may contribute to this initial “climatic” groundwater salinity, such as pumping inducing saltwater intrusion and mobilisation of brines [4, 11], high-efficiency irrigation systems producing high-salinity, low irrigation return rates [12], and misuse of fertilizers and agrochemicals, among others. For instance, the resulting groundwater salinity in many southern Europe coastal drylands exceed the standards of quality that the European Drinking Water Directive [13] recommends for human consumption and health, crop production, and survival of the ecosystems biodiversity [12].

In this context, agriculture has invariably had the highest freshwater demand [14, 15], contributing at growing of local societies, but accounting for 70% of withdrawals [16, 17]. The exposition of coastal aquifers to saltwater intrusion

(SWI) after disruption of natural conditions [18, 19] had reduced crop surface and therefore profit in many regions, with dramatic consequences for food production and social inequality. Users often forget that seawater is another water balance component. An unplanned exploitation is the cause behind the alteration of the fragile freshwater-saltwater equilibrium with typical consequences such as freshwater-saltwater mixing zone displacement inland and reduction of crop production. These anticipated negative indicators may end with abandonment of land devoted to irrigated crops.

Understanding coastal groundwater and irrigation farming interactions is a challenge because the equilibrium between sustainable pumping and agricultural profit is subjected to a fragile threshold determined by the crop-limiting salinity. This paper aims to contribute to this topic by means of a user-friendly programming tool that combines hydrological, agronomic, and economic components of the system [20, 21]. This multidisciplinary tool must deal with the complex network of variables that conform feedback loops subjected to delays and nonlinear relationships. For this, SD modelling is a very suitable approach. When the scope of the study goes beyond the academic field and aims to involve stakeholders and land-use planners, it is essential to link these models to DSS. These are software systems that integrate models, databases, or other decision aids and package them in a way that decision makers can use [22].

The perception of the complex interaction between the sociocultural, economic, and biophysical components of the systems is the cause of the growing interest in environmental DSSs [22–24]. This paper presents a Vensim application (Venapp) for the AQUACOAST simulation model, which aims to evaluate the sustainability of coastal groundwater-dependent agriculture. As described, the great threat to coastal aquifers is saltwater intrusion triggered by excessive freshwater pumping. Analyzing under what scenarios such a disaster may occur is the purpose of this simulation tool.

2. Materials and Methods

2.1. System Dynamics Modelling. SD modelling [25] is an ideal framework to integrate variables coming from different disciplines because it is based on a holistic view of the system under study and considers the model structure as a whole. SD modelling embodies system thinking through the implementation of differential equation systems. It is grounded in the theory of nonlinear dynamics and feedback control developed in mathematics, physics, and engineering.

A SD model is a stock-and-flow structure of first-order differential equations, which is commonly deterministic and used to generate the time trajectories of the model variables under different simulation scenarios. The model structure is made up of causal feedback loops, which include nonlinear relationships and delays, and constitute a holistic and easily overlooked because of its behavior [26].

Strong points of SD may be summarized as follows [27]: (i) SD models are useful learning tools that help improve system understanding and foster system thinking skills and knowledge integration for modelers and end users. This is true even for their first stage of development, i.e., as conceptual models. (ii)

Advances in the development of high-level dynamic modelling software platforms have made computational SD modelling more accessible. (iii) SD literature has made rich contributions to approaches informing on the modelling process, including data collection methods, knowledge elicitation/mapping techniques, and policy analysis.

The integrated models that allow the implementation of SD are essential to address environmental problems [28–30]. The degradation of the environment is forged by the imbalance created between the natural rate of regeneration of resources and their rate of exploitation, which is due to socioeconomic factors. In order to understand how economic systems are decoupled from natural ones and to seek sustainable solutions, it is essential to analyze the dynamic interactions between economic and natural biophysical systems [21, 31].

Advances in the development of high level dynamic modelling software platforms, such as iThink (isee systems, <http://www.iseesystems.com>), Vensim (Ventana Systems, <http://www.vensim.com>), and Powersim Studio (Powersim Software AS, <http://www.powersim.com>), have rendered computer SD models very accessible (even with minimal technical background). These applications are often designed as communication layers: user interface, stock-flow, mathematical equations, and programming code [27].

The important feature of these modelling tools is that they allow the user to write a model, even a complex one, without writing a single equation. The advantage is that the model diagram is focused on the relationships among the different variables and processes in the system and can be understood by a person with a good background in the problem domain of the model, but with little knowledge of mathematics. Models are designed “visually” by connecting blocks and aggregating them at different levels of resolution [22] what makes these tools very useful in the model prototyping phase and for educational purposes.

From all available options, we chose Vensim [32]. Although the software lacks certain possibilities, for example, does not support spatial treatment and its graphical interface is improvable [33], it is very suitable for the purpose we aim, to understand the typical functioning complexity of a coastal groundwater-dependent agricultural system subjected to different water-competing sectors and land-use policies. Complexity departs from the lack of data in many groundwater systems [34], thus complicating numerical modelling. There may be unknown essential information, such as the actual groundwater stored in an aquifer. In addition, cause and effect are separated in time and space which adds difficulty in conceptualizing basic hydrological processes. For instance, aquifer recharge may take place tens to hundreds of kilometers from the discharge area and may occur months to years before this water is pumped [4, 8].

2.2. Vensim Applications: Venapps. Interaction with simulation models has improved considerably in recent years. However, it can still be difficult for a nonexpert user to deal directly with programs such as Vensim. Friendly user interfaces are essential to involve nonmodeling experts in exploiting and improving models. The VensimDSS® software

[35] includes the possibility of developing simple Venapps to visualize the model structure, examine its causality, simulate the model behavior, and visualize its results [36–38].

Venapps are simplified, push-button interfaces that allow users access to a Vensim model without going through the Vensim modelling environment. A Venapp uses a model and a set of rules for interacting with the model to give users simplified access to that model. To the user, the Venapp appears as a series of buttons, menus, or a sequence of screens allowing him or her to use and analyze the model in straightforward and meaningful way.

The goal of these interactive simulators is to provide the user with the following tasks: examine the model structure, establish simulation scenarios, simulate the model, and analyze the impact of decisions on the behavior of the system under study. The VensimDSS environment includes an extension called Vensim application (VenappTM) which allows the creation of graphical user interfaces in the file format “vpa” (Vensim packaged application). Both model and Venapp can be run with the software “Vensim Model Reader” which can be downloaded from the Vensim® homepage for free (<http://www.vensim.com/freedownload.html>).

3. AQUACOAST Model

3.1. Overall Description. The AQUACOAST model implements the two-dimensional saltwater-freshwater interface (SFI) analytical solution proposed in [39] for an idealized unconfined (i.e., its upper boundary is the fluctuating water table) coastal aquifer, which is horizontal, enough thick, and overlying an impervious bedrock, isotropic, and hydraulically homogeneous with steady inflow (aquifer recharge) and outflow (aquifer discharge) rates (Figure 1). The variables and parameters of the AQUACOAST model concerning irrigation practices, groundwater hydrology, and groundwater allotment for agriculture have been added to the schematization of Verruijt [39]. In the steady schema of Verruijt [39], the SFI position is reached automatically

depending on the fresh groundwater flow. AQUACOAST modifies this hypothesis by introducing delays in order to reach the equilibrium described by Verruijt, which magnitude differs, which differ for the intrusion phase (minor delay) and the freshening phase (longer delay) [40]. Groundwater allotment for agricultural use is the main flow component. The model focuses on determining critical distances of agronomic interest from the shoreline, such as the current and equilibrium freshwater and salinization boundaries or the irrigation farming abandonment boundary (Figure 1).

AQUACOAST is a lumped spatial model [27], and thus, its variables represent either totals or averages over the entire area modelled. For the sake of illustration, the simulation period is 50 years, an appropriate time horizon when studying environmental degradation that can only be detected when observed the evolution of “slow variables” [41]. Variables and parameters use the SI units, capital letters being variables, whereas small letters denote parameters. Tables 1 and 2 include the notation, units, and adopted values for variables and parameters, respectively, after data from [4, 8, 20, 21, 40, 42, 43] and references therein. The AQUACOAST model uses 26 straightforward formulations divided into seven sections as follows.

3.2. Net Aquifer Discharge. One of the main hypotheses of the AQUACOAST model is that fresh groundwater flow moves towards the sea and discharges at the shoreline in natural regime. Net aquifer discharge (TDFW) is expressed as difference in inflow and outflow water balance components and is measured per unit thickness of the aquifer. In a disturbed regime, the model assumes that TDFW decreases due to groundwater pumping and the SFI displaces inland. The depth and extent of the SFI determine the fraction of usable fresh groundwater. The time-zero TDFW responds to initial pumping. This initial TDFW can be used to set other initial states in the AQUACOAST model. TDFW is expressed as

$$\text{TDFW}_t = \frac{[\text{appt} \cdot (1 - \text{cfro}) - \text{aaet} - \text{PUMP}_t \cdot (1 - \text{cfrf})] \cdot \text{lgth}}{365} + \frac{(\text{lttf} \cdot 10^3)}{(\text{wdth} \cdot 365)}, \quad (1a)$$

$$\text{TDFW}_0 = \frac{[\text{appt} \cdot (1 - \text{cfro}) - \text{aaet} - \text{PUMP}_0 \cdot (1 - \text{cfrf})] \cdot \text{lgth}}{365} + \frac{(\text{lttf} \cdot 10^3)}{(\text{wdth} \cdot 365)}, \quad (1b)$$

where TDFW = net aquifer discharge, PUMP = groundwater pumping, appt = annual precipitation, cfro = runoff coefficient, aaet = annual actual evapotranspiration, cfrf = return flow coefficient, lgth = coastal aquifer length, lttf = lateral groundwater transference from others aquifers, wdth = coastal aquifer width, t = state of the system at a given time, and 0 = time zero.

3.3. Saltwater and Freshwater Boundaries Dynamics. Verruijt [39] arrives at the formulae giving the depth of the SFI below sea level (h_s) and the height of the free groundwater surface (FGS: water table) (h_F) as functions of the shoreline distance along x -axis, TDFW, and three constants: hydraulic conductivity (cfpm), freshwater density (dtfw), and saltwater density (dtsw). Note that x , h_s , and h_F ,

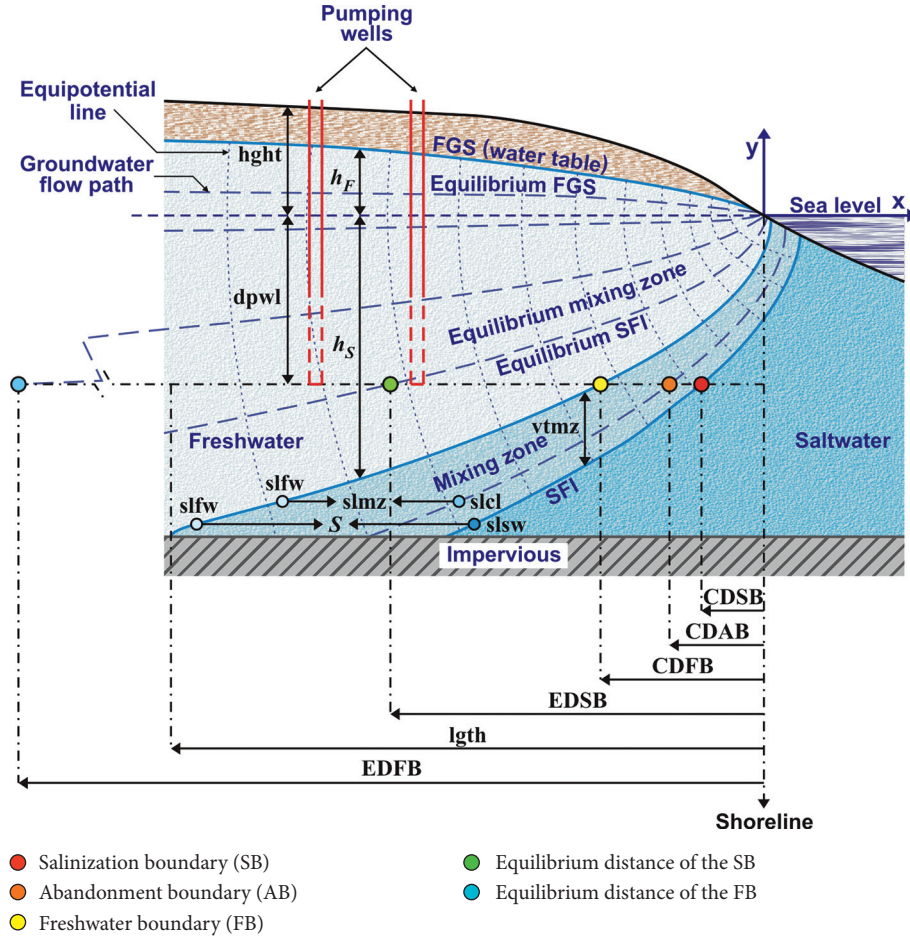


FIGURE 1: The AQUACOAST model added to Verruijt's schematization for an idealized unconfined coastal aquifer. h_F is the height of the free groundwater surface (FGS: water table) above sea level (it is not a model parameter), h_S is the depth of the saltwater-freshwater interface (SFI) below sea level (it is not a model parameter), h_{ght} is the average height of land surface above sea level, $vtmz$ is the vertical thickness of the mixing zone, $dpwl$ is the depth of pumping wells below sea level, CDSB is the current distance of the SB from the shoreline, CDAB is the current distance of the AB from the shoreline, CDFB is the current distance of the FB from the shoreline, EDSB is the equilibrium distance of the SB from the shoreline, EDFB is the equilibrium distance of the FB from the shoreline, $lgth$ is the coastal aquifer length, $slfw$ is the freshwater salinity, S is the mixing water salinity along the x -axis distance from the shoreline ($CDSB \leq x \leq CDFB$), $slmz$ is the actual average salinity across a line segment connecting FB and AB ($CDAB \leq x \leq CDFB$), $slcl$ is the crop-limiting salinity, and $slsw$ is the saltwater salinity.

TABLE 1: Notation for variables used.

Variable	Equation	Definition	Units ¹
ARIR	15, 26	Current irrigated area	$m^{-2} \cdot day^{-1}$
ARPI	11, 13	Potential irrigated area	$m^3 \cdot ha^{-1} \cdot year^{-1}$
ARTI	13, 15	Target for the irrigated area	$\epsilon \cdot year^{-1}$
CDAB	8, 11, 14, 19	Current distance of the AB from the shoreline	$m^3 \cdot ha^{-1} \cdot year^{-1}$
CDFB	5, 7, 8, 19	Current distance of the FB from the shoreline	$\epsilon \cdot ha^{-1} \cdot year^{-1}$
CDSB	3, 6, 7, 8, 14	Current distance of the SB from the shoreline	$\epsilon \cdot m^{-3}$
CHFW	10, 20	Current average height of the FGS above sea level	m
CSTW	20, 21, 24	Water cost per cubic meter	m
EDFB	4, 5	Equilibrium distance of the FB from the shoreline	$m^3 \cdot ha^{-1} \cdot year^{-1}$
EDSB	2, 3, 6, 14	Equilibrium distance of the SB from the shoreline	$m^3 \cdot ha^{-1} \cdot year^{-1}$
EHFW	9, 10	Equilibrium average height of the FGS above sea level	km
EXPF	13, 22	Expected profit per irrigated farm	km
EXWX	23, 25	Expected water requirement for profit maximization	km
IRDS	17, 21, 23, 26	Irrigation dose from groundwater	km
PFTH	21, 22	Profit per hectare	km
PPIR	16, 17, 23	Contribution of direct precipitation to irrigation	$year^{-1}$

TABLE 1: Continued.

Variable	Equation	Definition	Units ¹
PUMP	1, 26	Groundwater pumping	dmnl
RAIA	14, 15	Rate of abandonment of irrigated area	ha
S(x)	7, 18	Salinity of mixing water along the x-axis distance from the shoreline, $CDSB \leq x \leq CDFB$	kg·m ⁻³
SLFT	17, 18, 19, 24	Salinity factor	ha
TDFW	1, 2, 4, 9	Net aquifer discharge	ha
TMBE	3, 5, 6, 14	Time for the SB and FB to achieve equilibrium	year
WRXP	24, 25	Water requirement for profit maximization	mm·year ⁻¹
YLDH	17, 21	Crop yield per surface unit	kg·ha ⁻¹ ·year ⁻¹

1 – dmnl = dimensionless; ha = hectare; € = EU Euros.

TABLE 2: Notation for parameters used.

Parameter	Equation	Definition	Units ¹	Value ²
aaet	1	Annual actual evapotranspiration	mm·year ⁻¹	200
appt	1, 16	Annual precipitation	mm·year ⁻¹	300
arfr	15, 22	Area of one farm	ha	2.84
cdap	7, 8, 19	Calibration parameter to represent nonlinear variations in salinity	dmnl	3
cfpm	2, 4, 9	Hydraulic conductivity	m·day ⁻¹	10
cfrr	1	Return flow coefficient	dmnl	0.2
cfro	1, 16	Runoff coefficient	dmnl	0.2
cwot	20	Costs of water other than energy	€·m ⁻³	1.4
dpwl	2, 4	Depth of pumping wells below sea level	m	100
dtcp	2, 4, 9	Density contrast parameter	dmnl	0.025
dtfw	2, 4, 9	Freshwater density	kg·m ⁻³	1.000
dtsw	2, 4, 9	Saltwater density	kg·m ⁻³	1.025
efir	21, 24, 26	Irrigation system efficiency	dmnl	0.8
egcm	20	Energy required to pump one cubic meter one meter	kwh·m ⁻⁴	0.017
expf	22	Initial expected profit per irrigated farm	€·year ⁻¹	23,000
hght	20	Average height of land surface above sea level	m	100
idqt	23	Irrigation quota	m ³ ·ha ⁻¹ ·year ⁻¹	20,000
lgth	1, 2, 4, 9, 11, 14, 19, 26	Coastal aquifer length	km	10
lttf	1	Lateral transference from other aquifers	hm ³ ·year ⁻¹	7.9
oaag	16	If 1, then open-air agriculture else under plastic agriculture	dmnl	0
ocfm	13	Average opportunity cost for a farmer	€·yr ⁻¹	23,000
ocfv	13	Coefficient of variation of the opportunity cost for a farmer	dmnl	0.29
octh	21	Other costs per hectare	€·ha ⁻¹ ·year ⁻¹	40,053
prcp	21, 24	Crop price	€·kg ⁻¹	0.76
preg	20	Price of energy	€·kwh ⁻¹	0.05
pxys	23	If 1, then farmers seek economic optimum else they seek agronomic optimum	dmnl	1
pycm	17, 24	Potential marginal yield per cubic meter of water	kg·m ⁻³	30
sfmz	19	Average salinity factor across a line segment connecting the FB and AB	kg·m ⁻³	imp
slcl	8, 18, 19	Crop-limiting salinity	kg·m ⁻³	2
slfp	18, 19	Crop-specific calibration parameter	kg·m ⁻³	0.5
slfw	7, 8, 19	Freshwater salinity	kg·m ⁻³	0.15
slmz	19	Actual average salinity across a line segment connecting FB and AB, $CDAB \leq x \leq CDFB$	kg·m ⁻³	imp
slsw	7, 8	Saltwater salinity	kg·m ⁻³	35
subh	21	Subsidies per hectare	€·ha ⁻¹ ·year ⁻¹	0
tfex	15, 22, 25	Time for farmers to adjust expectations	year	3
tmbf	6	Time for current SB and FB to achieve equilibrium, freshening phase	year	10
tmbi	6	Time for current SB and FB to achieve equilibrium, intrusion phase	year	5
tmhe	10	Time for the FGS to achieve equilibrium	year	5
vtmz	4	Vertical thickness of the MZ	m	20
wdth	1, 11, 26	Coastal aquifer width	km	4
wrao	17, 23, 24, 25	Water requirement for agronomic optimum yield	m ³ ·ha ⁻¹ ·year ⁻¹	7500
subscript 0		Time zero, initial state of the system	year	unt
subscript s		Time step	year	0.0078125
subscript t		State of the system at a given time	year	unt

1 – dmnl = dimensionless; ha = hectare, 104 m²; € = EU Euros; 2 – imp = intermediate modelling parameter; unt = undefined time start or span.

as such, are not variables of the AQUACOAST model despite that they are included in Figure 1 for illustrative purposes.

As a convenient simplification, the model assumes that the depth of all the pumping wells below sea level (dpwl) is the same (Figure 1). In real aquifers, pumping wells may show substantial differences in depth. In this case, dpwl will adopt the depth of the deepest one or the depth of other shallowest ones as the SFI rises due to progressive pumping.

Let us call salinization boundary (SB) the line, in theory parallel to the shoreline for an isotropic and hydraulically homogeneous aquifer (whose projection in Figure 1 is a point) where the SFI intersects the horizontal plane that

connects the bottom of pumping wells (whose projection in Figure 1 is a line). It may be thought that the distance of the SB from the shoreline could be obtained by equaling Verrijt's h_s to dpwl and solving for x . However, this would entail assuming that the SFI moves instantaneously, which is not the case in real aquifers. Therefore, it is assumed that the expression obtained as mentioned gives the equilibrium distance from the shoreline that the SB would reach given the TDFW (EDSB) as in Figure 1. This expression includes a MIN function that avoids EDSB to be greater than the coastal aquifer length, as follows:

$$\text{EDSB}_t = \text{MIN} \left\{ \text{lgth}, \left(\left[\frac{\text{dpwl}^2 \cdot \text{cfpm} \cdot \text{dtcp} \cdot (1 + \text{dtcp})}{(2 \cdot \text{TDFW}_t)} \right] - \left[\frac{\text{TDFW}_t \cdot (1 - \text{dtcp})}{(2 \cdot \text{dtcp} \cdot \text{cfpm})} \right] \right) \cdot 10^{-3} \right\}, \quad (2a)$$

$$\text{EDSB}_0 = \text{MIN} \left\{ \text{lgth}, \left(\left[\frac{\text{dpwl}^2 \cdot \text{cfpm} \cdot \text{dtcp} \cdot (1 + \text{dtcp})}{(2 \cdot \text{TDFW}_0)} \right] - \left[\frac{\text{TDFW}_0 \cdot (1 - \text{dtcp})}{(2 \cdot \text{dtcp} \cdot \text{cfpm})} \right] \right) \cdot 10^{-3} \right\}, \quad (2b)$$

$$\text{dtcp} = \frac{(\text{dtsw} - \text{dtfw})}{\text{dtfw}}, \quad (2c)$$

where EDSB = equilibrium distance of the SB from the shoreline, TDFW = net aquifer discharge, lgth = coastal aquifer length, dpwl = depth of pumping wells below sea level, cfpm = hydraulic conductivity, dtcp = density contrast parameter, dtsw = saltwater density, dtfw = freshwater density, t = state of the system at a given time, and 0 = time zero.

The AQUACOAST model assumes that the SB moves towards equilibrium following an exponential fitting. Thus, the current distance of the SB from the shoreline (CDSB) is given by a first-order linear negative feedback. As deduced, no pumping wells whose distance from the shoreline is less than CDSB take saltwater (Figure 1). It is assumed that, initially, the system is in the equilibrium associated with initial TDFW as follows:

$$\text{CDSB}_{t+s} = \text{CDSB}_t + s \cdot \left[\frac{(\text{EDSB}_t - \text{CDSB}_t)}{\text{TMBE}_t} \right], \quad (3a)$$

$$\text{CDSB}_0 = \text{EDSB}_0, \quad (3b)$$

where CDSB = current distance of the SB from the shoreline, EDSB = equilibrium distance of the SB from the shoreline, TMBE = time for the SB and FB to achieve equilibrium, t = state of the system at a given time, 0 = time zero, and s = time step.

The AQUACOAST model represents the mixing zone (MZ) between the interface and the freshwater body (at left of the interface in Figure 1). The MZ has a constant vertical thickness (vtmz) (Figure 1). Let us call freshwater boundary (FB) the line, in theory parallel to the shoreline for an isotropic and hydraulically homogeneous aquifer, where the upper-inland surface of the MZ intersects the horizontal plane connecting the bottom of pumping wells (Figure 1). The distance of the FB from the shoreline in the equilibrium associated with the current TDFW (EDFB) results from substituting dpwl by $\text{dpwl} + \text{vtmz}$ in equations (2a)–(2c) as follows:

$$\text{EDFB}_t = \text{MIN} \left\{ \text{lgth}, \left(\left[\frac{(\text{dpwl} + \text{vtmz})^2 \cdot \text{cfpm} \cdot \text{dtcp} \cdot (1 + \text{dtcp})}{(2 \cdot \text{TDFW}_t)} \right] - \left[\frac{\text{TDFW}_t \cdot (1 - \text{dtcp})}{(2 \cdot \text{dtcp} \cdot \text{cfpm})} \right] \right) \cdot 10^{-3} \right\}, \quad (4a)$$

$$\text{EDFB}_0 = \text{MIN} \left\{ \text{lgth}, \left(\left[\frac{(\text{dpwl} + \text{vtmz})^2 \cdot \text{cfpm} \cdot \text{dtcp} \cdot (1 + \text{dtcp})}{(2 \cdot \text{TDFW}_0)} \right] - \left[\frac{\text{TDFW}_0 \cdot (1 - \text{dtcp})}{(2 \cdot \text{dtcp} \cdot \text{cfpm})} \right] \right) \cdot 10^{-3} \right\}, \quad (4b)$$

where EDFB = equilibrium distance of the FB from the shoreline, TDFW = net aquifer discharge, lgth = coastal aquifer length, dpwl = depth of pumping wells below sea level, vtmz = vertical thickness of the MZ, cfpm = hydraulic

conductivity, dtcp = density contrast parameter, t = state of the system at a given time, and 0 = time zero.

Again, the AQUACOAST model assumes that the FB moves towards equilibrium following an exponential fitting.

Thus, the current distance of the FB from the shoreline (CDFB) is given by a first-order linear negative feedback. The two surfaces limiting the MZ would move at the same velocity, so equations (3a) and (3b) for CDSB and equations (5a) and (5b) for CDFB use the same average adjustment time. As deduced, no pumping wells whose distance from the shoreline is greater than CDFB take freshwater (Figure 1). It is assumed that, initially, the system is in the equilibrium associated with the current TDFW as follows:

$$\text{CDFB}_{t+s} = \text{CDFB}_t + s \cdot \left[\frac{(\text{EDFB}_t - \text{CDFB}_t)}{\text{TMBE}_t} \right], \quad (5a)$$

$$\text{CDFB}_0 = \text{EDFB}_0, \quad (5b)$$

where CDFB = current distance of the FB from the shoreline, EDFB = equilibrium distance of the FB from the shoreline, TMBE = time for the SF and SB to achieve equilibrium, t = state of the system at a given time, 0 = time zero, and s = time step.

The time needed for SB and FB to achieve equilibrium (TMBE) differs when saltwater is encroaching (intrusion phase) and when freshwater is rinsing the salinized aquifer (freshening phase) [40]. In real aquifers, the freshening phase is quite longer than the intrusion phase. This is the reason why saltwater encroached during the last global sea-level maximum may still remain in some coastal aquifers [4, 44]. The TMBE expression includes a conditional function to reflect this difference as

$$\text{TMBE}_t = \{\text{IF EDSB}_t > \text{CDSB}_t \text{ THEN tmbi ELSE tmbf}\}, \quad (6)$$

where TMBE = time for the SB and FB to achieve equilibrium, EDSB = equilibrium distance of the SB from the shoreline, CDSB = current distance of the SB from the shoreline, tmbi = time for current boundaries to achieve equilibrium, intrusion phase, tmbf = time for current boundaries to achieve equilibrium, freshening phase, and t = state of the system at a given time.

3.4. Water Salinity. Verruijt's analytical solution assumes that water salinity in the FB (at distance CDFB from the shoreline) equals freshwater salinity (slfw), whereas water salinity in the SB (at distance CDSB from the shoreline) equals saltwater salinity (slsw). The AQUACOAST model defines the water salinity as the mass fraction of total dissolved solids relative to the sample weight: pristine coastal fresh groundwater is around 0.2 kg m^{-3} [10, 45], fresh groundwater in yielded coastal aquifers is typically in the $0.2\text{--}0.5 \text{ kg m}^{-3}$ range [46], saltwater is 35 kg m^{-3} [47], and crop-limiting irrigation water is 2 kg m^{-3} [43]. Let us assume that mixing water salinity (S) along the x -axis distance from the shoreline ($\text{CDSB} \leq x \leq \text{CDFB}$) connecting SB and FB (Figure 1) is given by slsw and slfw as

$$S(x) = \text{slfw} + (\text{slsw} - \text{slfw}) \cdot \left[\frac{(\text{CDFB} - x)}{(\text{CDFB} - \text{CDSB})} \right]^{\text{cdap}}, \quad (7)$$

where S = mixing water salinity along the x -axis distance from the shoreline ($\text{CDSB} \leq x \leq \text{CDFB}$), slfw = freshwater salinity, slsw = saltwater salinity, CDFB = current distance of the FB from the shoreline, CDSB = current distance of the SB from the shoreline, and cdap = calibration parameter to represent nonlinear variations in salinity.

Once defined S and slfw, the distance of the abandonment boundary (AB) (CDAB) from the shoreline (Figure 1) is obtained by equaling equation 7 to the crop-limiting salinity (slcl), i.e., the maximum water salinity for crop production, and then solving for x . Note that no pumping well whose distance from the shoreline is less than CDAB (i.e., $\text{slfw} > \text{slcl}$) can use groundwater for irrigation (Figure 1). CDAB is expressed as

$$\text{CDAB}_t = \text{CDFB}_t - (\text{CDFB}_t - \text{CDSB}_t) \cdot \left[\frac{(\text{slcl} - \text{slfw})}{(\text{slsw} - \text{slfw})} \right]^{(1/\text{cdap})}, \quad (8)$$

where CDAB = current distance of the AB from the shoreline, CDFB = current distance of the SB from the shoreline, CDSB = current distance of the SB from the shoreline, slcl = crop-limiting salinity, slfw = freshwater salinity, slsw = saltwater salinity, cdap = calibration parameter to represent nonlinear variations in salinity, and t = state of the system at a given time.

3.5. Free Groundwater Surface. The FGS (water table) is not a horizontal plane in Verruijt's conceptualization (Figure 1). However, the AQUACOAST model only makes use of its average height above sea level. The expression giving such an average FGS in the equilibrium associated with the current TDFW (EHFW) results from integrating the water table height above sea level between 0 and the coastal aquifer length (lgth) and then dividing the result by lgth as

$$\text{EHFW}_t = \left[\frac{8 \cdot \text{dtcp} \cdot \text{TDFW}_t \cdot \text{lgth} \cdot 10^3}{(9 \cdot \text{cfpm} \cdot (1 + \text{dtcp}))} \right]^{(1/2)}, \quad (9a)$$

$$\text{EHFW}_0 = \left[\frac{8 \cdot \text{dtcp} \cdot \text{TDFW}_0 \cdot \text{lgth} \cdot 10^3}{(9 \cdot \text{cfpm} \cdot (1 + \text{dtcp}))} \right]^{(1/2)}, \quad (9b)$$

where EHFW = equilibrium average height of the FGS above sea level, TDFW = net aquifer discharge, lgth = coastal aquifer length, cfpm = hydraulic conductivity, t = state of the system at a given time, and 0 = time zero.

Once again, the current average height of the FGS (CHFW) is assumed to move towards equilibrium following an exponential fitting as

$$\text{CHFW}_{t+s} = \text{CHFW}_t + s \left[\frac{\text{EHFW}_t - \text{CHFW}_t}{\text{tmhe}} \right], \quad (10a)$$

$$\text{CHFW}_0 = \text{EHFW}_0, \quad (10b)$$

where CHFW = current average height of the FGS above sea level, EHFW = equilibrium average height of the FGS above sea level, tmhe = time for the FGS to achieve equilibrium,

t = state of the system at a given time, 0 = time zero, and s = time step.

3.6. Irrigated Area. The potential irrigated area (ARPI) is the land area over the coastal aquifer where a pumping well with depth $dpwl$ below sea level would take fresh groundwater whose salinity does not exceed the crop-limiting salinity, i.e., the area covered by distance $lgth$ -CDAB (Figure 1). ARPI is expressed as

$$ARPI_t = width \cdot (lgth - CDAB_t) \cdot 10^2, \quad (11)$$

where $ARPI$ = potential irrigated area, $CDAB$ = current distance of the AB from the shoreline, $width$ = coastal aquifer width, $lgth$ = coastal aquifer length, $hekm$ = hectare-to-square-kilometer conversion parameter, and t = state of the system at a given time.

Let us assume that a number of people own equally sized pieces of agricultural land over the coastal aquifer. These persons consider entering or leaving irrigated farming by comparing the average expected profit per irrigated farm (EXPF) with the returns from other alternative economic activities, i.e., with their respective opportunity costs. However, it takes some time for them to decide and carry out their plans. Additionally, suppose that the opportunity cost follows a generalized Rayleigh distribution across farmers, which is commonly used to analyze skewed data [48]. The cumulative distribution function of this distribution is generically expressed as

$$P(X \leq x) = 1 - \exp\left\{\frac{-x^2}{[A^2(C^2 + 1)]}\right\}. \quad (12)$$

In equation (12), X is the opportunity cost of a farmer and A and C are the mean and the coefficient of variation of the opportunity cost across farmers, respectively. Note that P , X , x , A , and C , such as, are not variables of the AQUACOAST model. In this way, $P(X \leq EXPF)$ is the fraction of owners whose opportunity cost is less than the average expected profit per irrigated farm, i.e., the fraction of owners that regard irrigation as profitable. But, given that farms are equally sized, $P(X \leq EXPF)$ is also the fraction of the potential irrigated area where irrigation is seen as profitable. Multiplying this fraction by the potential irrigated area, the target for the irrigated area (ARTI) is obtained as

$$ARTI_t = ARPI_t \cdot \left[1 - \exp\left\{\frac{-EXPF_t^2}{[ocfm^2 \cdot (ocfv^2 + 1)]}\right\}\right], \quad (13)$$

where $ARTI$ = target for the irrigated area, $ARPI$ = potential irrigated area, $EXPF$ = expected profit per irrigated farm, $ocfm$ = average opportunity cost for a farmer, $ocfv$ = coefficient of variation of the opportunity cost for a farmer, and t = state of the system at a given time.

If irrigated farms are uniformly distributed over the coastal aquifer (excluding the coastal fringe CDAB where $slfw > slcl$), the rate of abandonment of irrigated area (RAIA), because pumping wells take groundwater whose salinity exceeds the crop-limiting salinity, equals the rate of saltwater

encroachment. Thus, the expression of RAIA results from dividing the velocity of the SB displacement inland by the length of the potential irrigated area. RAIA will equal zero in the freshening phase, i.e., when $EDSB < CDSB$. The RAIA expression is

$$RAIA_t = \max\left\{0, \frac{[EDSB_t - CDSB_t]}{[TMBE_t \cdot (lgth - CDAB_t)]}\right\}, \quad (14)$$

where $RAIA$ = rate of abandonment of irrigated area, $EDSB$ = equilibrium distance of the SB from the shoreline, $CDSB$ = current distance of the SB from the shoreline, $TMBE$ = time for the SB and FB to achieve equilibrium, $CDAB$ = current distance of the AB from the shoreline, $lgth$ = coastal aquifer length, and t = state of the system at a given time.

The current irrigated area (ARIR) approaches towards the target for the irrigated area (ARTI) following an exponential fitting though some irrigated area is simultaneously abandoned when saltwater is encroaching, i.e., when $RAIA > 0$. The AQUACOAST model assumes that there is only one irrigated farm pumping from the aquifer at time zero. ARIR is expressed as

$$ARIR_{t+s} = ARIR_t + s \cdot \left[\frac{(ARTI_t - ARIR_t)}{t_{fex}} - RAIA_t \cdot ARIR_t\right], \quad (15a)$$

$$ARIR_0 = arfr, \quad (15b)$$

where $ARIR$ = current irrigated area, $ARTI$ = target for the irrigated area, $RAIA$ = rate of abandonment of irrigated area, t_{fex} = time for farmers to adjust expectations, $arfr$ = area of one farm, t = state of the system at a given time, and 0 = time zero.

3.7. Profit per Irrigated Farm. The parameter $oaag$ allows the user to define whether the AQUACOAST model represents an open-air ($oaag = 1$) or an under plastic agricultural system ($oaag \neq 1$). In the former case, precipitation contributes to irrigation, whereas, in the latter, it does not. The contribution of precipitation to irrigation (PPIR) is expressed as

$$PPIR_t = \{ \text{IF } oaag = 1 \text{ THEN } appt \cdot (1 - cfro) \cdot 10 \text{ ELSE } 0 \}, \quad (16)$$

where $PPIR$ = contribution of precipitation to irrigation; $oaag$ = if 1, then open-air agriculture else under plastic agriculture; $appt$ = annual precipitation; $cfro$ = runoff coefficient; $mmhe$ = cubic-meter-to-millimeter-per-hectare conversion parameter; and t = state of the system at a given time.

The crop yield per hectare (YLDH) is related to the sum of the irrigation dose from groundwater (IRDS) and the contribution of precipitation to irrigation (PPIR) by means of a logistic or parabolic function. The function involves a salinity factor that measures the negative effect of water salinity on crop yield and ranges between zero and one. It can be proved that, for any nonnull value of the salinity

TABLE 3: Files compiled in the AQUACOAST Venapp.

File	Type	Number	Description
AQUACOAST.vmf	Simulation model	1	The usual extension of a Vensim model is *.mdl. However, for Venapp programming, it must be saved in binary format (*.vmf).
AQUACOAST.vcd	Venapp	1	Vensim application.
Intro.vmf	Simulation model	1	Simulation model to explore Vensim options.
Intro.vcd	Venapp	1	Vensim application.
Intro.vgd	Vensim graph data		Customized graphs that allow displaying more than one variable, with more than one scale, on a single graph.
.vdf	Vensim data file	n	Contains results from a simulation, including scenario values; the name of the exercise () is provided by the user.
Default.vdf	Vensim data file	1	Contains results from a default simulation, including scenario values.

factor, crop yield is maximized when IRDS + PPIR equals the water requirement for agronomic optimum yield (wrao) as

$$YLDH_t = \text{pym} \cdot \text{SLFT}_t \cdot (\text{IRDS}_t + \text{PPIR}_t) \cdot \text{MAX} \left\{ 0, 1 - \left[\frac{(\text{IRDS}_t + \text{PPIR}_t)}{(2 \cdot \text{wrao})} \right] \right\}, \quad (17)$$

where YLDH = crop yield per surface hectare, SLFT = salinity factor, IRDS = irrigation dose from groundwater, PPIR = contribution of precipitation to irrigation, pym = potential marginal yield per cubic meter of water, wrao = water requirement for agronomic optimum yield, and t = state of the system at a given time.

The expression of the salinity factor (SLFT) combines two values of another salinity factor, the one given by [49]. This factor is generically expressed as

$$\text{SLFT} = \text{MAX} \left\{ 0, 1 - \text{MAX} \left\{ \frac{0, S - \text{slfp}}{(\text{slcl} - \text{slfp})} \right\} \right\}, \quad (18)$$

where SLFT = salinity factor generically expressed, S = mixing water salinity along the x-axis distance from the shoreline ($\text{CDSB} \leq x \leq \text{CDFB}$) as in equation 7, slcl = crop-limiting salinity, slfp = another crop-specific calibration parameter, and t = state of the system at a given time.

The first value of SLFT is one, its length is lgth - CDFB (Figure 1), and it corresponds to the freshwater zone where pumping wells take fresh groundwater. The second value of SLFT corresponds to the inland part of the MZ where pumping wells take salty groundwater still useful for crop production ($\text{slcl} \geq \text{slfw}$), and its length is CDFB - CDAB (Figure 1). Integrating equation 7 between CDAB and CDFB and then dividing the result by CDFB - CDAB gives the actual average salinity across the line segment connecting FB and AB (slmz). Thus, the value of SLFT in the second zone (slmz) results from using slmz instead of S in equation (19). Finally, SLFT is a weighted average of the two mentioned values of SLFT, where the weights are the lengths of the respective zones. Note that, in doing so, (1) the crop yield per hectare (YLDH) is also a weighted average of the crop yields corresponding to both zones, and (2) if salinity increased linearly along the line segment between CDAB and CDFB, i.e., if cdap = 1, slmz would be the simple average of the crop

limiting (slcl) and the freshwater (slfw) salinities. SLFT is expressed as

$$\text{SLFT}_t = \frac{[(\text{lgth} - \text{CDFB}_t) + \text{sfmz} \cdot (\text{CDFB}_t - \text{CDAB}_t)]}{(\text{lgth} - \text{CDAB}_t)}, \quad (19a)$$

$$\text{sfmz} = \text{MAX} \left\{ 0, 1 - \text{MAX} \left\{ \frac{0, \text{slmz} - \text{slfp}}{(\text{slcl} - \text{slfp})} \right\} \right\}, \quad (19b)$$

$$\text{slmz} = \text{slfw} + \frac{(\text{slcl} - \text{slfw})}{(\text{cdap} + 1)}, \quad (19c)$$

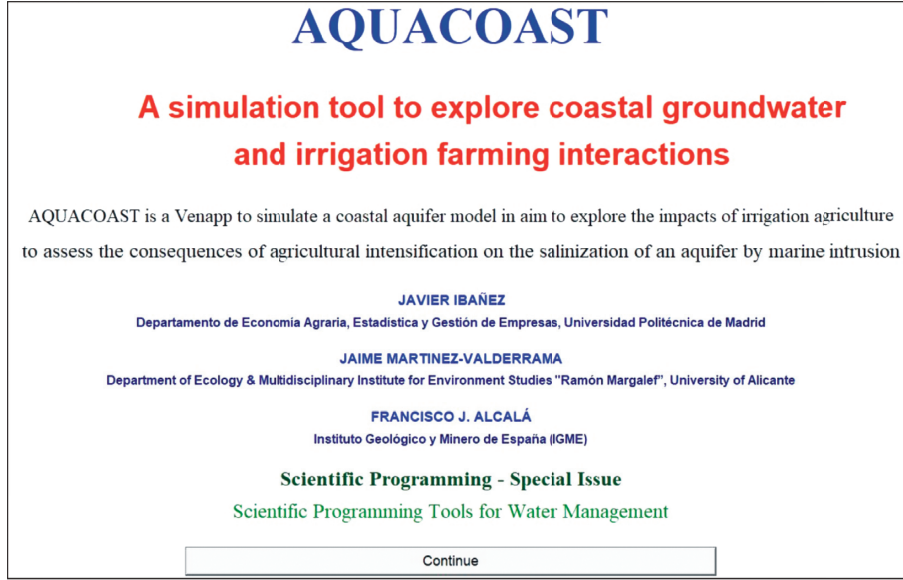
where YLDH = salinity factor, CDFB = current distance of the FB from the shoreline, CDAB = current distance of the AB from the shoreline, lgth = coastal aquifer length, sfmz = average salinity factor across a line segment connecting the FB and AB, slmz = actual water salinity across a line segment connecting the FB and AB ($\text{CDAB} \leq x \leq \text{CDFB}$), slfp = calibration parameter to represent nonlinear variations in salinity, slcl = crop-limiting salinity, slfw = freshwater salinity, and t = state of the system at a given time.

The cost of water per cubic meter (CSTW) combines the cost of the energy needed to pump groundwater, which depends on the FGS (water table) depth and the price of energy and other costs as

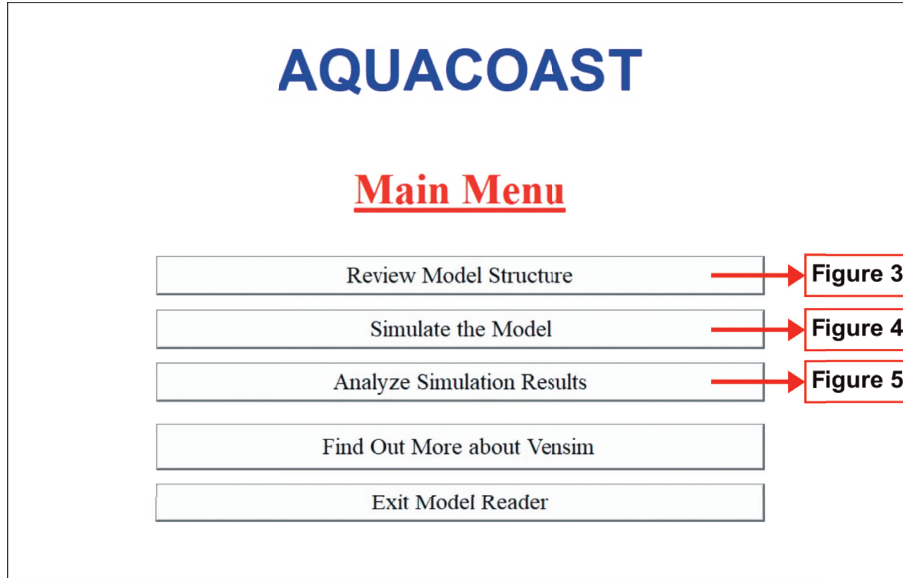
$$\text{CSTW}_t = \text{egcm} \cdot (\text{hght} - \text{CHFW}_t) \cdot \text{preg} + \text{cwot}, \quad (20)$$

where CSTW = water cost per cubic meter, CHFW = current average height of the FGS above sea level, egcm = energy required to pump one cubic meter one meter, hght = average height of land surface above sea level, preg = price of energy, cwot = costs of water other than energy, and t = state of the system at a given time.

The profit per hectare (PFTH) is the difference in incomes and costs per hectare. Incomes come from the selling of agricultural production and from subsidies. The costs per hectare are the cost of water and other costs. The former results from multiplying the water cost per cubic meter (CSTW) and the actual irrigation dose from groundwater (IRDS). This product tries to reach the desired irrigation dose over the efficiency of the irrigation system. Other costs



(a)



(b)

FIGURE 2: (a) Welcome screen of the AQUACOAST Venapp; (b) main menu screen.

per hectare are aggregated into a single model parameter (octh). PFTH is expressed as

$$PFTH_t = prcp \cdot YLDH_t + subh - \frac{(CSTW_t \cdot IRDS_t)}{efir - octh}, \quad (21)$$

where PFTH=profit per hectare, YLDH=crop yield per hectare, CSTW=water cost per cubic meter, IRDS=irrigation dose from groundwater, prcp=crop price, subh=subsidies per hectare, efir=irrigation system efficiency, octh=other costs per hectare, and t=state of the system at a given time.

The expected profit per irrigated farm (EXPF) results from multiplying the profit per hectare (PFTH) and the area of one farm (arfr). The AQUACOAST model implements the expectation about such a profit is a moving

average of observed past profits where weights exponentially decrease over time. This is the well-known exponential smoothing, which can be expressed as a first-order linear negative feedback [26] as

$$EXPF_{t+s} = EXPF_t + s \cdot \left[\frac{arfr \cdot PFTH_t - EXPF}{tfex} \right], \quad (22a)$$

$$EXPF_0 = expf, \quad (22b)$$

where EXPF=expected profit per irrigated farm, PFTH=profit per hectare, arfr=area of one farm, tfex=time for farmers to adjust expectations, expf=initial expected profit per irrigated farm, t=state of the system at a given time, 0=time zero, and s=time step.

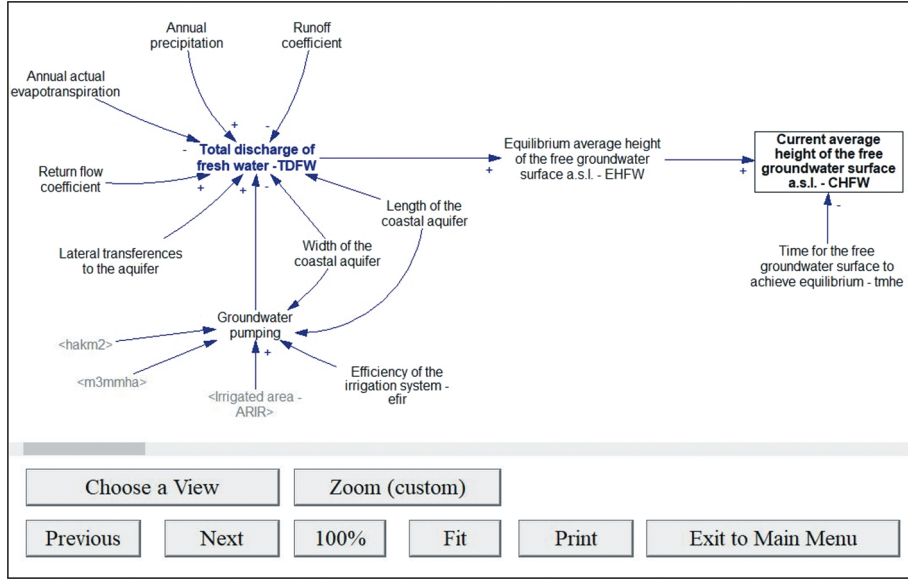


FIGURE 3: “Coastal aquifer dynamics” view of the AQUACOAST model.[[parms resize(1),pos(50,50),size(200,200),bgcol(156)]]

3.8. Groundwater Pumping. The AQUACOAST model includes the parameter $pxys$ that allows the user to define whether farmers seek to maximize the profit per irrigated farm ($pxys = 1$) or crop yield ($pxys \neq 1$). Note that the water requirement for each of these goals is different. In the latter case, the water requirement is given by the parameter $wrao$ as in equation (17). The expression of the expected water requirement for profit maximization (EXWX) will be given later. Whatever the case, the irrigation dose from groundwater (IRDS) is the difference in water requirement and contribution of precipitation to irrigation. The resultant irrigation dose cannot be greater than the irrigation quota, if any. The expression of the initial value of IRDS simply considers $EXWX = wrao$. IRDS is expressed as

$$IRDS_t = \text{MIN}\{\text{idqt}, \text{MAX}\{0, \{\text{IF } pxys = 1 \text{ THEN } EXWX_t \text{ ELSE } wrao\} - PPIR_t\}\}, \quad (23a)$$

$$IRDS_0 = \text{MIN}\{\text{idqt}, \text{MAX}\{0, wrao - PPIR_t\}\}, \quad (23b)$$

where $IRDS$ = irrigation dose from groundwater; $PPIR$ = contribution of precipitation to irrigation; $EXWX$ = expected water requirement for profit maximization; idqt = irrigation quota; $pxys$ = if 1, then farmers seek economic optimum else they seek agronomic optimum; $wrao$ = water requirement for agronomic optimum yield; t = state of the system at a given time; and 0 = time zero.

The water requirement for profit maximization (WRXP) results from calculating the partial derivative of equation (21) to deduce profit per hectare with respect to the irrigation dose, equaling it to zero, and then solving for the irrigation dose as

$$WRXP_t = wrao \cdot \left[\frac{1 - CSTW_t}{(efir \cdot prcp \cdot pycm \cdot SLFT_t)} \right], \quad (24)$$

where $WRXP$ = water requirement for profit maximization, $CSTW$ = water cost per cubic meter, $SLFT$ = salinity factor, $wrao$ = water requirement for agronomic optimum yield, $efir$ = irrigation system efficiency, $prcp$ = crop price, $pycm$ = potential marginal yield per cubic meter of water, and t = state of the system at a given time.

For the current year, farmers cannot know the water requirement for profit maximization because many of the factors involved are unknown a priori, e.g., crop and energy prices, or the incidence of salinization. However, farmers can form an approximation of such a water requirement for the current year ($EXWX$) by learning from past experiences. This learning process would follow an exponential fitting to the true water requirement for profit maximization. In the AQUACOAST model, the initial value of $EXWX$ is taken to be the water requirement for agronomic optimum yield, a technical parameter which is easier to grasp by farmers. $EXWX$ is expressed as

$$EXWX_{t+s} = EXWX_t + s \cdot \left[\frac{(WRXP_t - EXWX_t)}{tfex} \right], \quad (25a)$$

$$EXWX_0 = wrao, \quad (25b)$$

where $EXWX$ = expected water requirement for profit maximization, $WRXP$ = water requirement for profit maximization, $tfex$ = time for farmers to adjust expectations, $wrao$ = water requirement for agronomic optimum yield, t = state of the system at a given time, 0 = time zero, and s = time step.

Groundwater pumping (PUMP) results from multiplying the current irrigated area (ARIR) and the actual irrigation dose (IRDS) and then dividing by the coastal aquifer area as

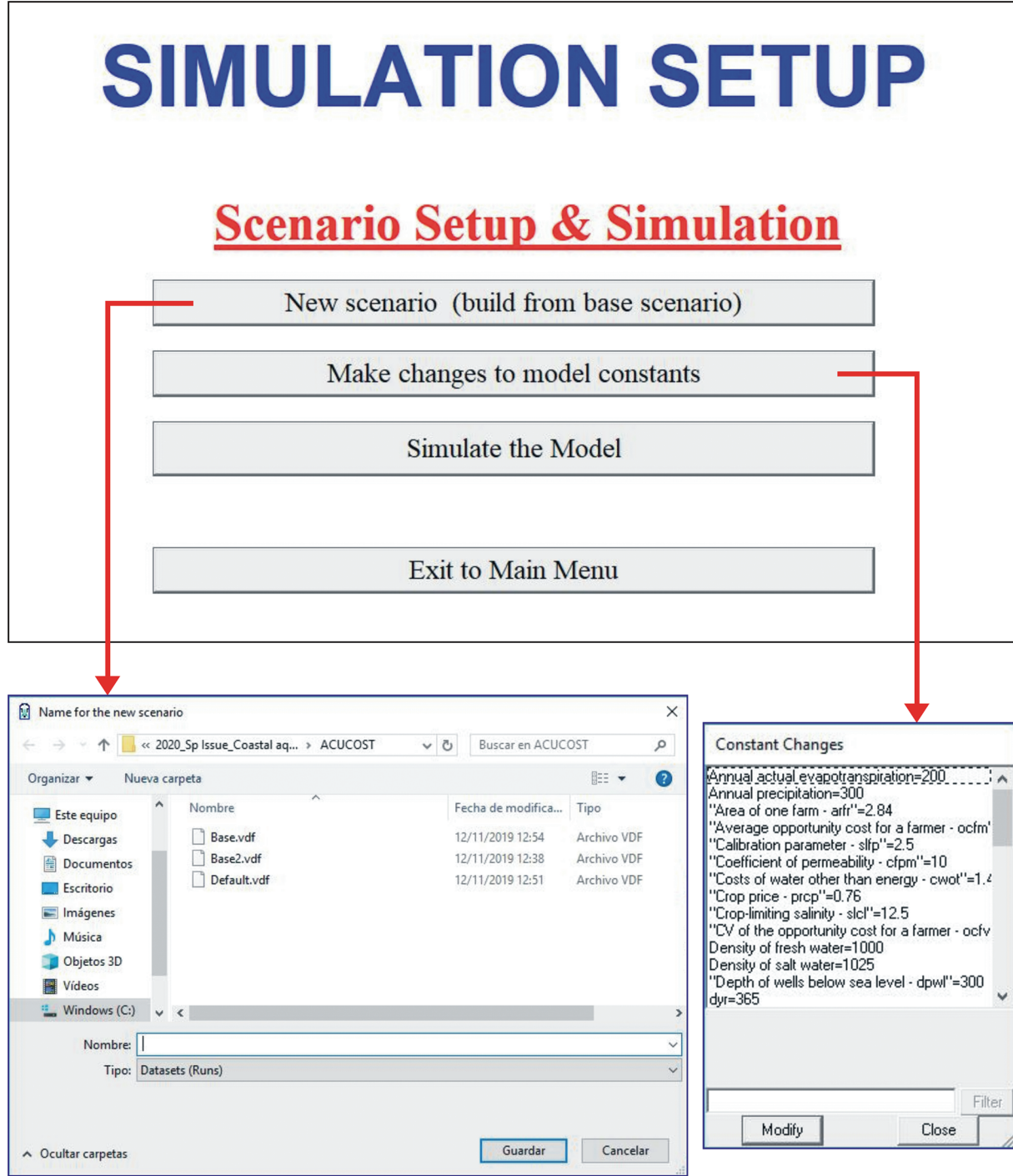


FIGURE 4: Simulation setup screen, including setting up and simulation scenarios.

$$PUMP_t = \frac{ARIR_t \cdot IRDS_t}{(width \cdot lgth \cdot efr \cdot 10^3)}, \quad (26a)$$

$$PUMP_0 = \frac{ARIR_0 \cdot IRDS_0}{(width \cdot lgth \cdot efr \cdot 10^3)}, \quad (26b)$$

where PUMP=groundwater allotment for irrigation, ARIR=current irrigated area, IRDS=irrigation dose from groundwater, width=coastal aquifer width, lgth=coastal

aquifer length, efr=irrigation system efficiency, t=state of the system at a given time, and 0=time zero.

4. AQUACOAST Venapp

4.1. Overall Description. The Vensim® DSS extension Venapps™ was utilized to program the user-friendly interface of the above described formulations. To use AQUACOAST, it is necessary to install Vensim Reader and

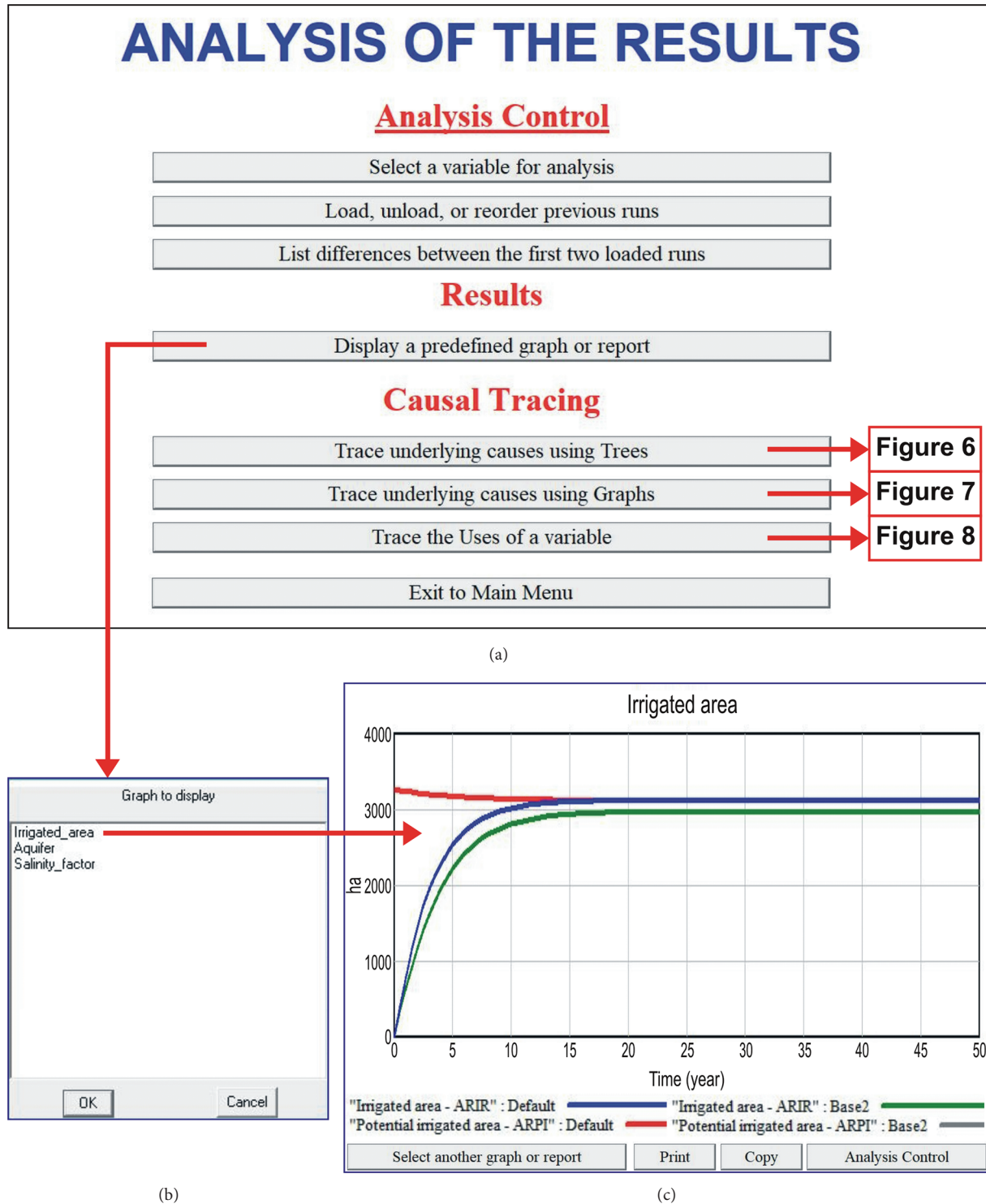


FIGURE 5: (a) “Analysis of the results” screen including three blocks: analysis control, results, and causal tracing; (b) for the “result” block, menu of available graphs; (c) temporal trends of the main variables for the default optional scenarios, in this example, “irrigated area.”

the folder with all the necessary files (Table 3) on the computer.

After opening the AQUACOAST file, the welcome screen will appear (Figure 2(a)). Here is brief information about the model and its authors. Clicking on the “Continue” button takes the user to the main menu (Figure 2(b)). From

this point, it is possible to (i) review the model structure, (ii) access the screen from which the simulation scenarios configured the model is executed, and (iii) analyze the results using different tools of Vensim. The bottom part of the screen gives the option to explore the possibilities offered by Vensim (button “Find Out More about Vensim”), which is

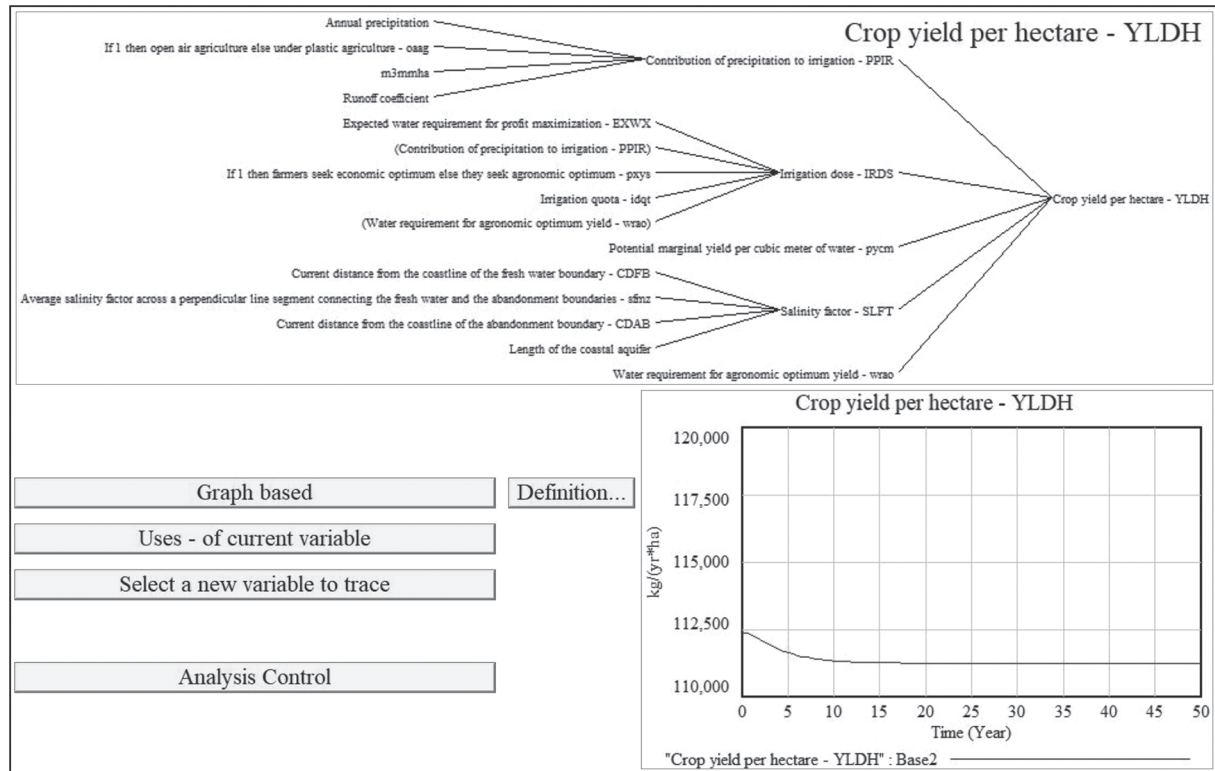


FIGURE 6: “Trace underlying causes with Trees” screen. Example of the underlying causes of “Crop yield per hectare” variable using trees.

supported by the Intro.vmf model file (Table 3) and is part of the Vensim examples, or leave the simulator (button “Exit Model Reader”).

4.2. Exploring the Structure of the Model. One of the main purposes of SD is to understand how a system works. To do this, Vensim offers multiple tools. The first allows studying the model structure. For this to be practical, the model must be split into different screens or “Views” by clicking the button “Review Model Structure” as in Figure 2(b) so that the user can gradually assimilate the relationship between the variables involved. Figure 3 shows one of these screens as an example. The button captions themselves explain the available utilities.

4.3. Running the Model. The button “Simulate the Model” as in Figure 2(b) enables the model to be executed. In this part of the Venapp (Figure 4), the simulation scenarios are set. For the former, the “New scenario. . .” button opens a dialog box to select an existing simulation or create a new one. After that, the “Make changes. . .” button will show all the model parameters and their default values; by modifying them, alternative scenarios will be created.

These changes are not permanent, for it would be necessary to access the model through a commercial license of Vensim® DSS and change them. Therefore, if the model is simulated without any modification, the user will obtain the results contained in the Default.vdf simulation file (Table 3). After setting the scenario, the

model is ready to be simulated. After clicking on the button to execute Vensim “Simulate the Model,” a blank screen will appear on which the user has to click to move on to the next stage, which consists of visualizing and analyzing the results.

4.4. Analyzing Results. After clicking button “Analyze Simulation Results” as in Figure 2(b), this stage offers three blocks of possibilities: analysis control, results, and causal tracing (Figure 5(a)). The “Analysis Control” block allows the user to manage simulations, select variables, and compare scenarios. This is a useful option when starting to accumulate simulations. In that case, it is hard to remember what changes from one scenario to another. Using the “Load, unload. . .” button, this option details which parameters change (and how much) between the two previously selected simulations.

The “Results” block displays predesigned graphs showing the temporal evolution of the most important variables of the model (Figure 5(a)). Clicking on the button “Display a predefined. . .,” a list will appear with the available graphics (Figure 5(b)). In all of them, the results of the default scenario will be included, as well as the results of the simulation that appear in the first position of the list of loaded simulations, which are managed from the “Load, unload, or reorder. . .” button, as in Figure 5(c).

The “Causal Tracing” block (Figure 5(a)) enables the use of Vensim’s own analysis tools, as shown in Figures 6–8. The tree diagram tool creates a graphical representation of the

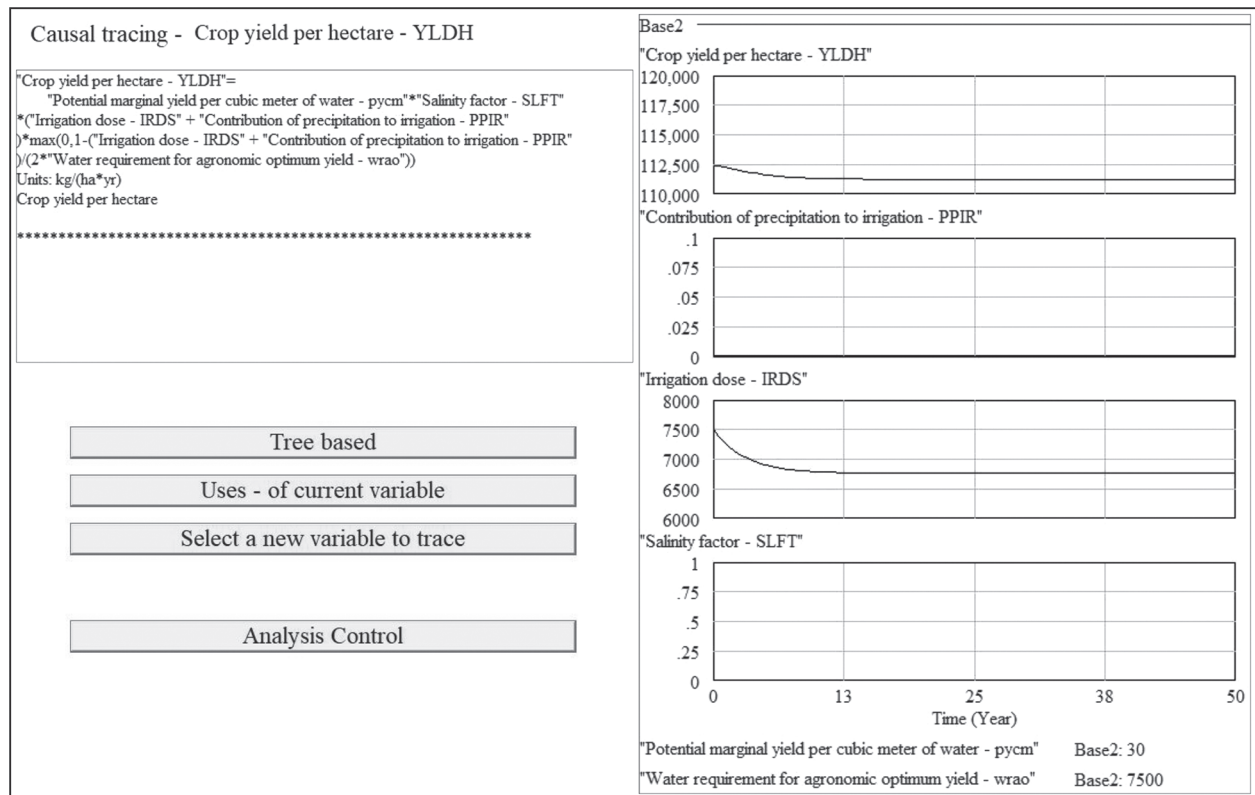


FIGURE 7: “Trace underlying causes with Graphs” screen. Example of the underlying causes of “Crop yield per hectare” variable using graphs.

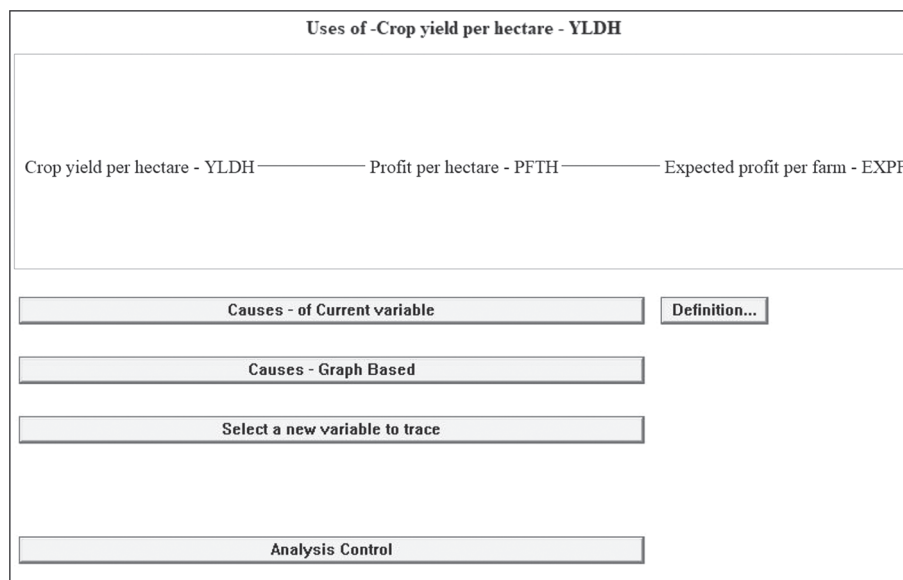


FIGURE 8: “Trace the Uses of a variable” screen. Example of the underlying causes of “Crop yield per hectare” variable.

structure of a model associated with the selected workbench variable; the currently active variable is displayed at the top left of the screen. The tree diagram tool provides an easy-to-read, graphical representation of the causes and uses of variables. This is a convenient way for displaying structural relationships and therefore information about a complex structure in a relatively small space.

The causal structure of the model can be explored using trees or charts, whereas the uses of each variable can only be analyzed using trees by displaying the tree of variables affected by the selected one. Figure 6 shows the screen that appears after clicking the button “Trace underlying causes using Trees.” At the top is the causal tree of the currently active variable. It is possible to select



FIGURE 9: Southern Mediterranean European groundwater bodies affected by saltwater intrusion due to overexploitation (modified from [55]).

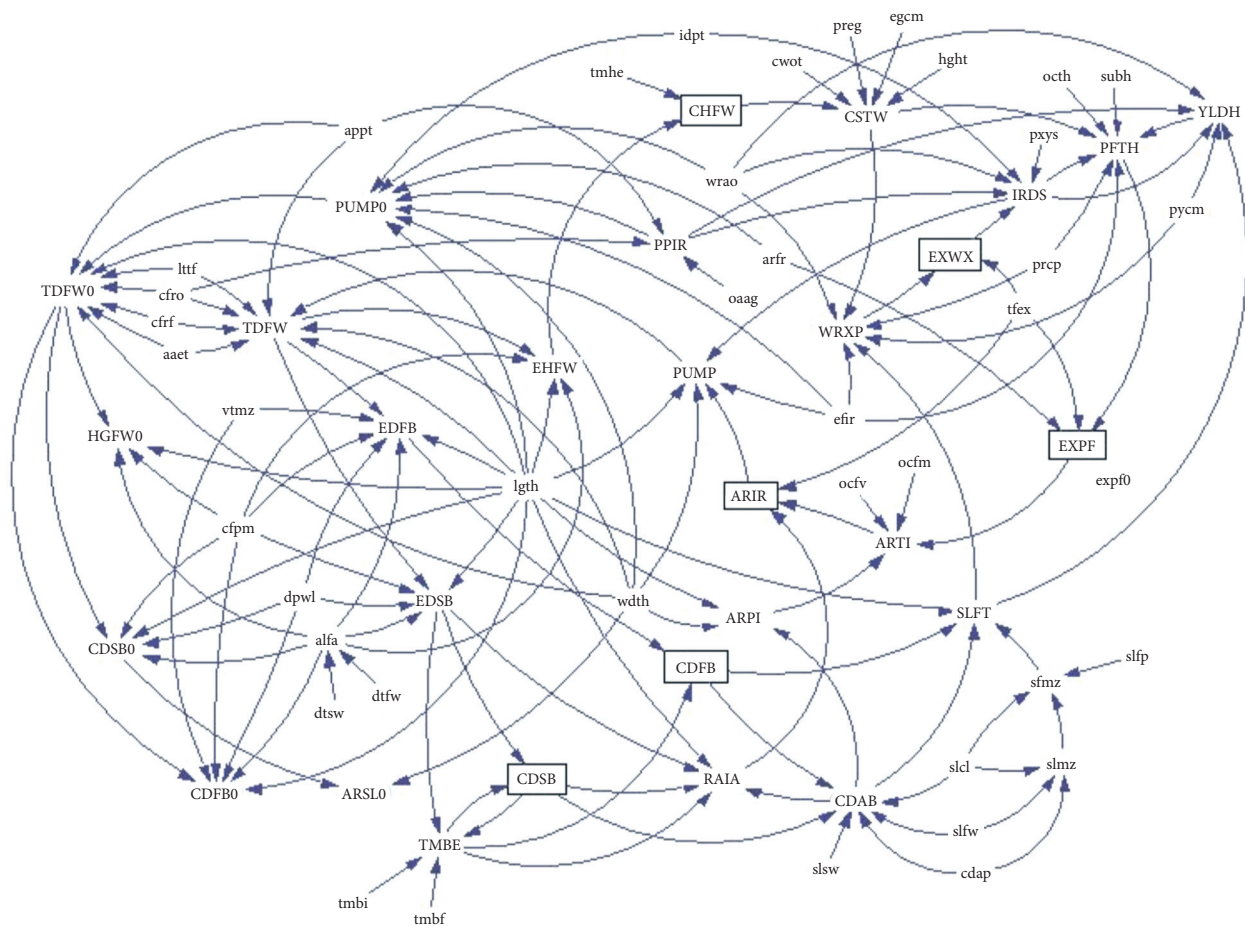


FIGURE 10: Original sketch of the AQUACOAST model. Acronyms for variables (capital letters) and parameters (small letters) are as in Tables 1 and 2, respectively.

other variables using the “Select a new variable...” button or, interactively, by clicking on any variable in the same causal tree. In addition, the user can (i) access to the model equations through the button “Definition...” and (ii) see its temporal trajectory according to the last simulated or loaded scenario. The rest of the buttons allow the user to scroll to other screens, as their own caption indicates. In this way, all the options of using the tree diagram tool are interconnected.

Clicking the button “Trace underlying causes using Graphs” (Figure 5(a)), the graphical option to study the causal tree of a variable can be used (Figure 7). In this case, only first-order variables, i.e., those directly affected by the selected variable, are shown. On the right side of the screen, the temporal trajectories of the variables included in the performance equation can be observed, as well as the value of the parameters involved. The definition of the variable is also presented in the box on the left. The rest of the options allow

the user to navigate between the screens related to the diagram tool.

The third analysis option offered by this Venapp (Figure 5(a)) is to “Trace the Uses of a variable” (Figure 8). Again, it is possible to see its definition and scroll to other analysis screens. Finally, it is important to highlight the interactivity of the tree diagram tool. Any of the outputs it generates allows the user to select a new variable by clicking on it. This option is designed to make it easier to explore and study the model, one of Vensim’s hallmarks.

5. Discussion and Conclusions

5.1. Global Relevance of Coastal Groundwater Resources. Groundwater is one of the more strategic renewable resources, especially in coastal drylands [4]. Over two billion people rely on groundwater as their primary potable freshwater source [50], whereas half or more of the irrigation water used for food production has also this source [17]. Groundwater also acts as the key strategic reserve in times of drought [51] and to set population in drylands with sparse economic options except agriculture [8, 20].

Soaring water withdrawal worsens water scarcity already prevalent in those coastal drylands having limited surface water resources. A consequence of the aquifer overexploitation to cope with water requirements is saltwater intrusion, which threatens the sustainable food production and economic development in an increasing number of countries [15, 52, 53].

The use of SD modelling in water management has a long tradition due to the complex nature of the problems addressed [54]. However, few models consider the interaction between terrestrial water fluxes and human activities and associated uses, and even fewer are the models intended to coastal groundwater-dependent irrigation agriculture [15]. The AQUACOAST tool is a contribution to fill this gap of knowledge.

The AQUACOAST is a global application tool despite that the Mediterranean region is postulated as a main scenario in which to apply. Coastal aquifers in this area support strong groundwater pumping rates for crop production, and saltwater intrusion has extended in most of them (Figure 9). For instance, in Spain, this problem affects most of the Mediterranean coastal aquifers, so they were considered one of the “desertification landscapes” in the National Program to Combat Desertification [56, 57]. Our immediate purpose is to apply AQUACOAST to coastal aquifers of the Mediterranean arc where tourist and agricultural pressure has triggered problems of marine intrusion such as Campo de Dalías, Campo de Níjar, Vélez River and Verde River in Spain, Martíl-Alila and Smir in Morocco, and Nador and Tipaza in Argelia.

5.2. Using SD for Modelling Coastal Groundwater-Dependent Irrigation Systems. SD models express in mathematical language (the most precise way that exists) the dynamic processes that take place in a given field of study. The academic and scientific value of understanding how many variables relate, determining what is cause and what is effect, making explicit

feedback loops of a system, and, finally, translating them into a set of operative differential equations is very high.

However, it is important to make an additional effort so that this information reaches the less specialized public involved in decision-making processes. In order to do this, the use of DSSs is essential. An example taken from AQUACOAST can help us understand the value of programming an application aimed at a wider audience. Figure 10 shows the causal diagram drawn up for purely academic use as an indecipherable amalgam in the eyes of someone other than the modeler. Variables are represented by acronyms, and it is difficult to follow the path of causality in the complex web of causal relationships. However, a careful edition of the model, expliciting the full name of each variable and splitting the diagram into five screens (Figure 3 shows one of them), allows the user to create a much more user-friendly version.

The precision of mathematical language should not confuse us about the nature of the SD models. In reality, when confronted with socioecological systems, we lack universal physical or chemical laws that allow us to talk about predictions. Socioecological systems require input from a wide range of sources and types of knowledge [58]. This includes qualitative and quantitative pieces on information from various stakeholder groups such as scientists, policy makers, and community members. To collect, synthesize, and use these datasets in useful ways, integrated assessment and modelling needs to utilize and combine different methods (i.e., conceptual, numerical, and participatory) in appropriate methodological designs that best fit the project’s context, objective, and constraints, in the latter case including resource availability [27, 33].

The AQUACOAST model is not intended for prediction or forecasting, even though they provide outputs over variable time periods. This is because there are not enough data to validate the models for such purposes; remember, for example, the lack of some essential information such as the initial groundwater storage or similar others like past weather data or former land uses. Thus, the aim is to get qualitative rather than quantitative outputs, answering the “what if” questions, which helps to compare simulation scenarios that address different hypotheses.

System understanding and experimentation also constitute important goals of the models, as well as social learning, though this is limited to those cases where the assessment shows a special risk of degradation. Since degradation usually proceeds slowly, stakeholders are not sufficiently aware of its consequences, no matter how they value the water and land use being degraded [59]. Thus, the AQUACOAST model is intended as a “means of exploration” [60, 61] for helping them to better understand how a coastal groundwater-dependent agricultural system may behave.

5.3. The AQUACOAST Venapp. Just as there are several SD modelling platforms, DSS can be built using a wide range of possibilities. Venapps offer clear advantages when the software chosen is VensimDSS. The construction is very fast since there are templates that with few modifications allow

the user to implement the main options of a DSS: configuration of scenarios, simulation, and visualization of the results and their analysis. The use of the tool is simple since it only requires to install the free version of VensimDSS (Vensim Reader) and to copy the Vensim files provided by the modeler.

The main problem is the graphical limitation of Vensim, which prevents the use of images or figures or the implementation of options such as global sensitivity analysis or risk estimation. More complex DSS based on Vensim can be built using various programming languages (e.g., Visual Basic) and platforms (e.g., Excel), such as the application designed by authors to study desertification risk in Spain, which combined some hotspots such as soil erosion, grassland overgrazing, and aquifer overexploitation [57]. However, the choice of the type of DSS depends, as does the construction of a model, on its purpose.

Since the AQUACOAST tool is aimed at (i) facilitating the study and understanding of coastal groundwater-dependent irrigated agriculture systems and (ii) creating an application whose installation and use are very simple, Venapp is a perfect ally since it makes available to the user, in a very simple way, all the analysis tools of Vensim.

Since Meadows et al. [62] presented the revolutionary best-seller “Limits to growth,” for which they used systems thinking and SD concepts in order to explain how short-term development policies can lead to “overshoot and collapse” behavior of socioecological systems, SD has shown its potential as a tool to help understand complex socioecological systems and is still regarded as a valuable resource for thinking about sustainable futures [33, 63]. The AQUACOAST tool is in line with these principles and aims to highlight the fragility of such a strategic renewable resource as groundwater. As long as the model describes reality with a certain accuracy, the modelling process and its outcomes can be used to improve our understanding of the problem of excessive pumping under the increasing food production needs a necessary step towards affecting sustainable and effective change [64].

Data Availability

The labeled dataset used to support the findings of this study are available from the corresponding author upon request.

Conflicts of Interest

The authors declare that there are no conflicts of interest regarding the publication of this paper.

Acknowledgments

This study was funded by the European Research Council grant agreement no. 647038 (BIODESERT).

References

- [1] C. Small and R. J. Nicholls, “A global analysis of human settlement in coastal zones,” *Journal of Coastal Research*, vol. 19, pp. 584–599, 2003.
- [2] J. S. Famiglietti, “The global groundwater crisis,” *Nature Climate Change*, vol. 4, no. 11, pp. 945–948, 2014.
- [3] R. J. Naiman, J. J. Magnuson, D. M. McKnight, J. A. Stanford, and J. R. Karr, “Freshwater ecosystems and their management: a national initiative,” *Science*, vol. 270, no. 5236, pp. 584–585, 1995.
- [4] E. Custodio, “Coastal aquifers of Europe: an overview,” *Hydrogeology Journal*, vol. 18, no. 1, pp. 269–280, 2010.
- [5] E. Custodio, J. M. Andreu-Rodes, R. Aragón et al., “Groundwater intensive use and mining in south-eastern peninsular Spain: hydrogeological, economic and social aspects,” *Science of The Total Environment*, vol. 559, pp. 302–316, 2016.
- [6] S. Sabater and D. Barceló, *Water Scarcity in the Mediterranean. Perspectives under Global Change*, Springer-Verlag, Berlin, Germany, 2010.
- [7] C. Dalin, Y. Wada, T. Kastner, and M. J. Puma, “Groundwater depletion embedded in international food trade,” *Nature*, vol. 543, no. 7647, pp. 700–704, 2017.
- [8] F. J. Alcalá, M. Martín-Martín, F. Guerrero, J. Martínez-Valderrama, and P. Robles-Marín, “A feasible methodology for groundwater resource modelling for sustainable use in sparse-data drylands: application to the Amtoudi Oasis in the northern Sahara,” *Science of The Total Environment*, vol. 630, pp. 1246–1257, 2018.
- [9] P. Baudron, F. Barbecot, J. L. G. Aróstegui, C. Leduc, Y. Travi, and D. Martínez-Vicente, “Impacts of human activities on recharge in a multilayered semiarid aquifer (Campo de Cartagena, SE Spain),” *Hydrological Processes*, vol. 28, no. 4, pp. 2223–2236, 2014.
- [10] F. J. Alcalá and E. Custodio, “Spatial average aquifer recharge through atmospheric chloride mass balance and its uncertainty in continental Spain,” *Hydrological Processes*, vol. 28, no. 2, pp. 218–236, 2014.
- [11] E. Custodio, W. M. Edmunds, and Y. Travi, “Management of coastal palaeowaters,” in *Paleowaters in Coastal Europe: Evolution of Groundwater since the Late Pleistocene*, W. M. Edmunds and C. J. Milne, Eds., vol. 189, pp. 313–327, Geological Society. Special Publications, London, UK, 2001.
- [12] M. Rodríguez-Rodríguez, J. Benavente, F. J. Alcalá, and M. Paracuellos, “Long-term water monitoring in two Mediterranean lagoons as an indicator of land-use changes and intense precipitation events (Adra, Southeastern Spain),” *Estuarine, Coastal and Shelf Science*, vol. 91, no. 3, pp. 400–410, 2011.
- [13] European Union, “Council Directive 98/83/EC of 3 November 1998 on the quality of water intended for human consumption,” *Official Journal of the European Union*, vol. 330, pp. 32–54, 1998.
- [14] B. Scanlon, C. Faunt, L. Longuevergne et al., “Groundwater depletion and sustainability of irrigation in the US high plains and central valley,” *Proceedings of the National Academy of Sciences*, vol. 109, no. 24, pp. 9320–9325, 2012.
- [15] Y. Wada, D. Wisser, and M. F. P. Bierkens, “Global modeling of withdrawal, allocation and consumptive use of surface water and groundwater resources,” *Earth System Dynamics*, vol. 5, no. 1, pp. 15–40, 2014.
- [16] P. Döll and S. Siebert, “Global modeling of irrigation water requirements,” *Water Resources Research*, vol. 38, no. 4, 2002.
- [17] S. Siebert, J. Burke, J. M. Faures et al., “Groundwater use for irrigation—a global inventory,” *Hydrology and Earth System Sciences*, vol. 14, no. 10, pp. 1863–1880, 2010.
- [18] D. M. FitzGerald, M. S. Fenster, B. A. Argow, and I. V. Buynevich, “Coastal impacts due to sea-level rise,”

- Annual Review of Earth and Planetary Sciences*, vol. 36, no. 1, pp. 601–647, 2008.
- [19] V. E. A. Post, “Fresh and saline groundwater interaction in coastal aquifers: is our technology ready for the problems ahead?” *Hydrogeology Journal*, vol. 13, no. 1, pp. 120–123, 2005.
 - [20] F. J. Alcalá, J. Martínez-Valderrama, P. Robles-Marín et al., “A hydrological-economic model for sustainable groundwater use in sparse-data drylands: application to the Amtoudi Oasis in southern Morocco, northern Sahara,” *Science of The Total Environment*, vol. 537, pp. 309–322, 2015.
 - [21] J. Martínez-Valderrama, J. Ibáñez, F. J. Alcalá, A. Dominguez, M. Yassin, and J. Puigdefábregas, “The use of a hydrological-economic model to assess sustainability in groundwater-dependent agriculture in drylands,” *Journal of Hydrology*, vol. 402, no. 1–2, pp. 80–91, 2011.
 - [22] A. E. Rizzoli and W. J. Young, “Delivering environmental decision support systems: software tools and techniques,” *Environmental Modelling & Software*, vol. 12, no. 2–3, pp. 237–249, 1997.
 - [23] M. Matthies, C. Giupponi, and B. Ostendorf, “Environmental decision support systems: current issues, methods and tools,” *Environmental Modelling & Software*, vol. 22, no. 2, pp. 123–127, 2007.
 - [24] J. D. Sterman and L. B. Sweeney, “Cloudy skies: assessing public understanding of global warming,” *System Dynamics Review*, vol. 18, no. 2, pp. 207–240, 2002.
 - [25] J. W. Forrester, *Industrial Dynamics*, The MIT Press, Cambridge, UK, 1961.
 - [26] J. D. Sterman, *Business Dynamics: Systems Thinking and Modeling for a Complex World*, McGraw-Hill, New York, NY, USA, 2000.
 - [27] R. A. Kelly, A. J. Jakeman, O. Barreteau et al., “Selecting among five common modelling approaches for integrated environmental assessment and management,” *Environ. Model. Softw.*, vol. 47, pp. 159–181, 2013.
 - [28] J. Ibáñez, J. Martínez-Valderrama, and J. Puigdefábregas, “Assessing overexploitation in Mediterranean aquifers using system stability condition analysis,” *Ecological Modelling*, vol. 218, no. 3–4, pp. 260–266, 2008.
 - [29] J. Martínez-Valderrama, J. Ibáñez, G. Del Barrio et al., “Doomed to collapse: why Algerian steppe rangelands are overgrazed and some lessons to help land-use transitions,” *Science of The Total Environment*, vol. 613–614, pp. 1489–1497, 2018.
 - [30] J. M. Fernández and M. A. E. Selma, “The dynamics of water scarcity on irrigated landscapes: mazarrón and Aguilas in south-eastern Spain,” *System Dynamics Review*, vol. 20, no. 2, pp. 117–137, 2004.
 - [31] T. Uehara, Y. Nagase, and W. Wakeland, “Integrating economics and system dynamics approaches for modelling an ecological-economic system,” *Systems Research and Behavioral Science*, vol. 33, no. 4, pp. 515–531, 2015.
 - [32] R. L. Eberlein, D. W. Peterson, V. Systems, and J. G. Road, “Understanding models with Vensim,” *European Journal of Operational Research*, vol. 59, no. 1, pp. 216–219, 1992.
 - [33] S. Elsawah, S. A. Pierce, S. H. Hamilton et al., “An overview of the system dynamics process for integrated modelling of socio-ecological systems: lessons on good modelling practice from five case studies,” *Environmental Modelling & Software*, vol. 93, pp. 127–145, 2017.
 - [34] M. Moench, J. Burke, and Y. Moench, “Rethinking the approach to groundwater and food security,” vol. 24, FAO, Rome, Italy, 2003, Water Reports.
 - [35] Ventana Systems Inc., *VensimDSS*, Ventana Systems Inc., Harvard, MA, USA, 2019.
 - [36] Y. Barlas and V. Dicker, “Decision support for strategic university management: a dynamic interactive game,” in *Proceedings of the International System Dynamics Conference*, Istanbul, Turkey, August 1997.
 - [37] P. Pfaffenbichler, “Modelling with systems dynamics as a method to bridge the gap between politics, planning and science? Lessons learnt from the development of the land use and transport model MARS,” *Transport Reviews*, vol. 31, no. 2, pp. 267–289, 2011.
 - [38] P. A. Walker, R. Greiner, D. McDonald, and V. Lyne, “The Tourism Futures Simulator: a systems thinking approach,” *Environmental Modelling & Software*, vol. 14, no. 1, pp. 59–67, 1998.
 - [39] A. Verruijt, “A note on the ghyben-herzberg formula,” *International Association of Scientific Hydrology. Bulletin*, vol. 13, no. 4, pp. 43–46, 1968.
 - [40] E. Giménez-Forcada, “Space/time development of seawater intrusion: a study case in Vinaroz coastal plain (Eastern Spain) using HFE-Diagram, and spatial distribution of hydrochemical facies,” *Journal of Hydrology*, vol. 517, pp. 617–627, 2014.
 - [41] J. F. Reynolds, D. M. S. Smith, E. F. Lambin et al., “Global desertification: building a science for dryland development,” *Science*, vol. 316, no. 5826, pp. 847–851, 2007.
 - [42] R. G. Allen, L. S. Pereira, D. Raes, and M. Smith, *Crop Evapotranspiration: Guidelines for Computing Crop Water Requirements. Irrigation and Drainage*, Food and Agriculture Organization, Rome, Italy, 1998.
 - [43] R. S. Ayers and D. Westcot, *Water Quality for Agriculture. Irrigation and drainage paper 29*, Food and Agriculture Organization, Rome, Italy, 1985.
 - [44] H. Kooi, J. Groen, and A. Leijnse, “Modes of seawater intrusion during transgressions,” *Water Resources Research*, vol. 36, no. 12, pp. 3581–3589, 2000.
 - [45] E. Dahl, “Ecological salinity boundaries in poikilohaline waters,” *Oikos*, vol. 7, no. 1, pp. 1–21, 1956.
 - [46] H. A. Swenson and H. L. Baldwin, *A Primer on Water Quality*, USGS. Department of Interior, Washington, DC, USA, 1965.
 - [47] W. Stumm and J. J. Morgan, *Aquatic Chemistry, Chemical Equilibria and Rates in Natural Waters*, John Wiley & Sons, New York, NY, USA, 3rd edition, 1996.
 - [48] M. Z. Raqab and M. T. Madi, “Generalized Rayleigh distribution,” in *International Encyclopedia of Statistical Science*, M. Lovric, Ed., Springer Berlin Heidelberg, Berlin, Germany, pp. 599–603, 2011.
 - [49] R. Aragües, *Manejo de los suelos. Interpretación. Caso particular de salinización y sodificación. Correcciones.*, *Jornada Técnica del Colegio Oficial de Ingenieros Técnicos Agrícolas de Lérida “Fertilización y Riego: Aplicaciones en Fruticultura*, Colegio Oficial de Ingenieros Técnicos Agrícolas de Lérida, Lleida, Spain, 2011.
 - [50] W. M. Alley, R. W. Healy, J. W. LaBaugh, and T. E. Reilly, “Flow and storage in groundwater systems,” *Science*, vol. 296, pp. 1985–1990, 2002.
 - [51] J. S. Famiglietti, M. Lo, S. L. Ho et al., “Satellites measure recent rates of groundwater depletion in California’s Central Valley,” *Geophysical Research Letters*, vol. 38, pp. 2–5, 2011.
 - [52] P. Döll, K. Fiedler, and J. Zhang, “Global-scale analysis of river flow alterations due to water withdrawals and reservoirs,” *Hydrology and Earth System Sciences*, vol. 13, no. 12, pp. 2413–2432, 2009.

- [53] M. Kummu, P. J. Ward, H. De Moel, and O. Varis, "Is physical water scarcity a new phenomenon? Global assessment of water shortage over the last two millennia," *Environmental Research Letters*, vol. 5, pp. 1–10, 2010.
- [54] P. P. Rogers and M. B. Fiering, "Use of systems analysis in water management," *Water Resources Research*, vol. 22, no. 9S, pp. 146S–158S, 1986.
- [55] European Environment Agency (EEA), "The European environment: state and outlook 2005," Technical Report No 1/2005, European Environment Agency (EEA), Copenhagen, Denmark, 2005.
- [56] MAGRAMA, *Programa de Acción Nacional contra la Desertificación*, MAGRAMA, Madrid, Spain, 2008.
- [57] J. Martínez-Valderrama, J. Ibáñez, G. Del Barrio et al., "Present and future of desertification in Spain: implementation of a surveillance system to prevent land degradation," *Science of The Total Environment*, vol. 563–564, pp. 169–178, 2016.
- [58] A. J. Jakeman, R. A. Letcher, and J. P. Norton, "Ten iterative steps in development and evaluation of environmental models," *Environmental Modelling & Software*, vol. 21, no. 5, pp. 602–614, 2006.
- [59] J. Ibáñez, J. F. L. Contador, S. Schnabel, M. P. Fernández, and J. Martínez-Valderrama, "A model-based integrated assessment of land degradation by water erosion in a valuable Spanish rangeland," *Environmental Modelling & Software*, vol. 55, pp. 201–213, 2014.
- [60] T. Oxley, B. McIntosh, N. Winder, M. Mulligan, and G. Engelen, "Integrated modelling and decision-support tools: a Mediterranean example," *Environmental Modelling & Software*, vol. 19, no. 11, pp. 999–1010, 2004.
- [61] G. L. W. Perry and J. D. A. Millington, "Spatial modelling of succession-disturbance dynamics in forest ecosystems: concepts and examples," *Perspectives in Plant Ecology, Evolution and Systematics*, vol. 9, no. 3-4, pp. 191–210, 2008.
- [62] D. Meadows, D. Meadows, J. Randers, and W. W. Behrens III, *The Limits to Growth*, Universe Books, New York, NY, USA, 1972.
- [63] G. M. Turner, "On the cusp of global collapse? Updated comparison of the limits to growth with historical data," *GAIA—Ecological Perspectives for Science and Society*, vol. 21, no. 2, pp. 116–124, 2012.
- [64] I. Winz, G. Brierley, and S. Trowsdale, "The use of system dynamics simulation in water resources management," *Water Resources Management*, vol. 23, no. 7, pp. 1301–1323, 2009.